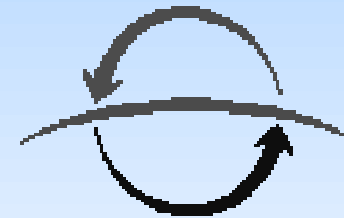


Implications of Measured Commercial Building Loads on Geothermal System Sizing

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EPRI



Overview

- Purpose & Objectives
 - quantify loads and load diversity in Geothermal applications
- Describe test sites, data collection, and analysis methods
- Compare measured loads from each site
- Implications for geothermal loop sizing

Objectives

- Analyze measured heating and cooling load data from several commercial buildings to:
 - determine peak loads and load diversity
 - determine full load cooling and heating hours
- Compare load characteristics of various building applications
- Show the implications of measured loads on geothermal loop sizing

Monitored Buildings

Sun Prairie, WI Office Building



Middleton, WI Office Building



Geneva, NY Hotel



Johnson City, TN High School



Buildings Characteristics

| | Sun Prairie Office Building | Middleton Office Building | Geneva Hotel | Johnson City High School |
|-----------------------------|-----------------------------|--|---|---------------------------------------|
| <i>Building</i> | | | | |
| Building Description: | two-story office | seven-story office | 149 room hotel | high school |
| Building Size: | 27,000 ft ² | 76,000 ft ² (86% w/ WLHPs) | 100,000 ft ² | 161,600 ft ² |
| Installed Capacity: | 69 tons | 146 tons | 284 tons | 400 tons |
| Floor Area per ton: | 391 ft ² /ton | 448 ft ² /ton | 352 ft ² /ton | 400 ft ² /ton |
| Construction Date | 1990 | 1990 | 1997 | 1995 (renovation) |
| <i>Heat Pumps</i> | | | | |
| No. of Heat Pumps: | 30 | 54 | 198 | 118 |
| Average EER (ARI 320) | 11.4 Btu/Wh | 11.4 Btu/h | 14.8 Btu/Wh | 14.5 Btu/Wh |
| <i>Loop Pumps</i> | | | | |
| Number and Size: | (2) 5 HP pumps | (2) 15 HP pumps | (3) 50 HP pumps | (2) 40 HP pumps |
| Flow Rate: | 200 gpm (2.9 gpm/ton) | 475 gpm (3.3 gpm/ton) | 810 gpm (2.5 gpm/ton) | 1,200 gpm (3 gpm/ton) |
| Norm. Pump Power | 0.072 HP/ton | 0.010 HP/ton | 0.31 HP/ton | 0.20 hp/ton |
| Pump Control | Constant Speed | Constant Speed | Variable Speed | Dual Two-Speed (staged: ½, 1, 2) |
| <i>Ground Loop</i> | | | | |
| Ground Loop | na | na | 198 pilings, 85 ft deep (33,660 ft) 120 bores, 138 ft deep (33,120 ft) | 320 Bores, 150 ft deep (96,000 ft) |
| Norm. Loop Size | na | na | 103 ft of bore/ton | 120 ft of bore/ton |
| <i>Cooling Tower</i> | | | | |
| Type | fluid cooler | fluid cooler | na | na |
| Cooling Fan: | 20 HP fan, 2-speed | 20 HP fan, 2-speed | na | na |
| Design Capacity: | 1.0 million Btu/h | 1.4 million Btu/h | na | na |
| <i>Boiler</i> | | | | |
| Input | 500,000 Btu/h | 962,000 Btu/h | na | na |

Monitored Data Collected

- Hotel (NY)
 - measured loop heat rejection/extraction... flow-delta-T (5-min data)
- Offices (WI)
 - measured total HP power (kWh) & loop temperatures (15-min data)
- High School (TN)
 - measured loop heat rejection/extraction... flow delta-T (60-min data)
 - measured heating/cooling status of each heat pump

Office Methodology



- Used measured loop loading & assumed COPs to calculate heating and cooling loads

$$Q_{cooling} = [measured _ kW] \cdot COP_c(T)$$

$$Q_{heating} = [measured _ kW] \cdot COP_h(T)$$

where: $COP_{c,h}(T)$ = HP efficiency as a function of loop supply temperature T

Hotel Methodology



- Used measured loop loading & assumed COPs to calculate heating and cooling loads

$$Q_{cooling} = Q_{rejection} \cdot \frac{COP_c(T)}{COP_c(T) + 1}$$

$$Q_{heating} = Q_{extraction} \cdot \frac{COP_h(T)}{COP_h(T) - 1}$$

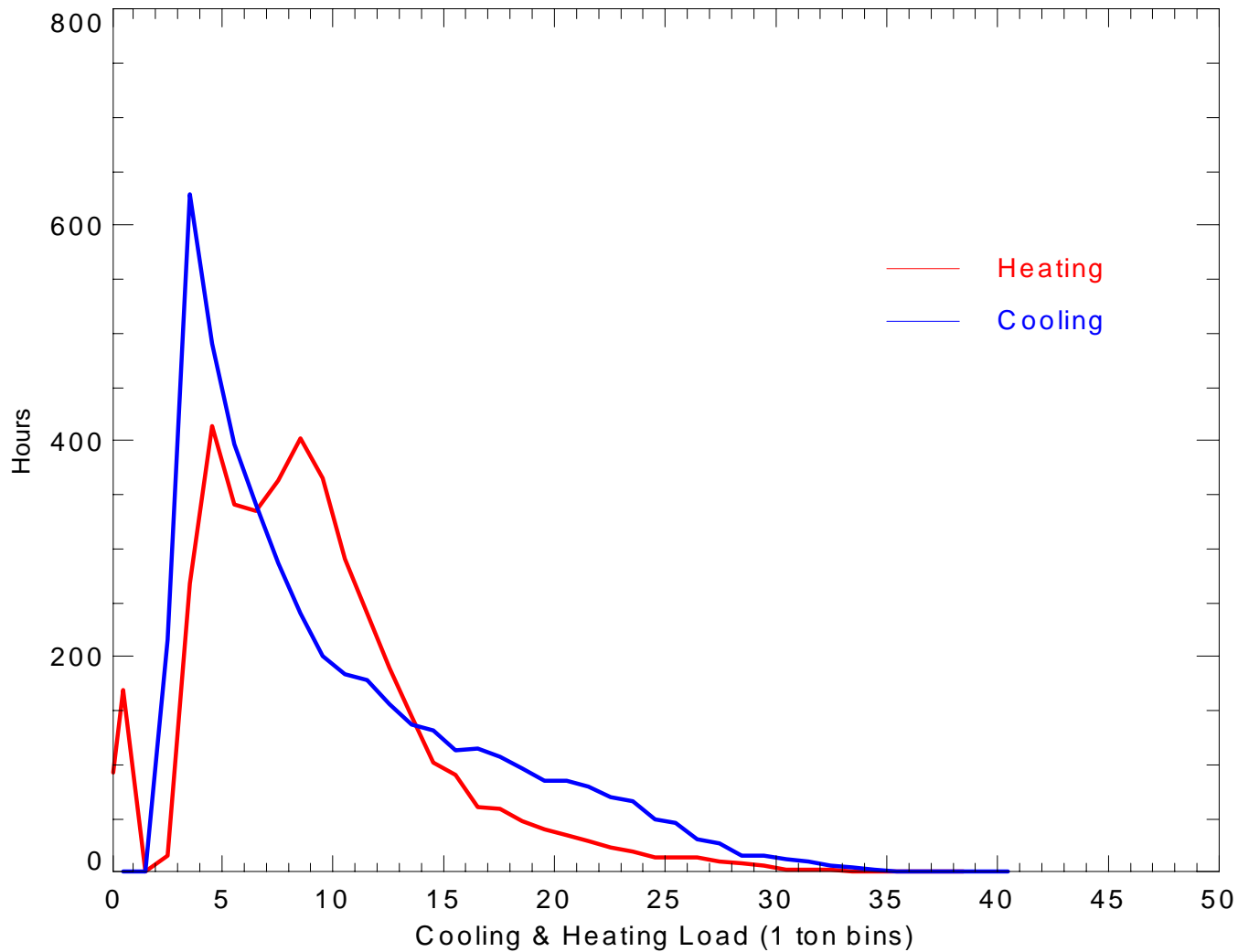
where: $COP_{c,h}(T)$ = HP efficiency as a function of loop supply temperature T

School Methodology

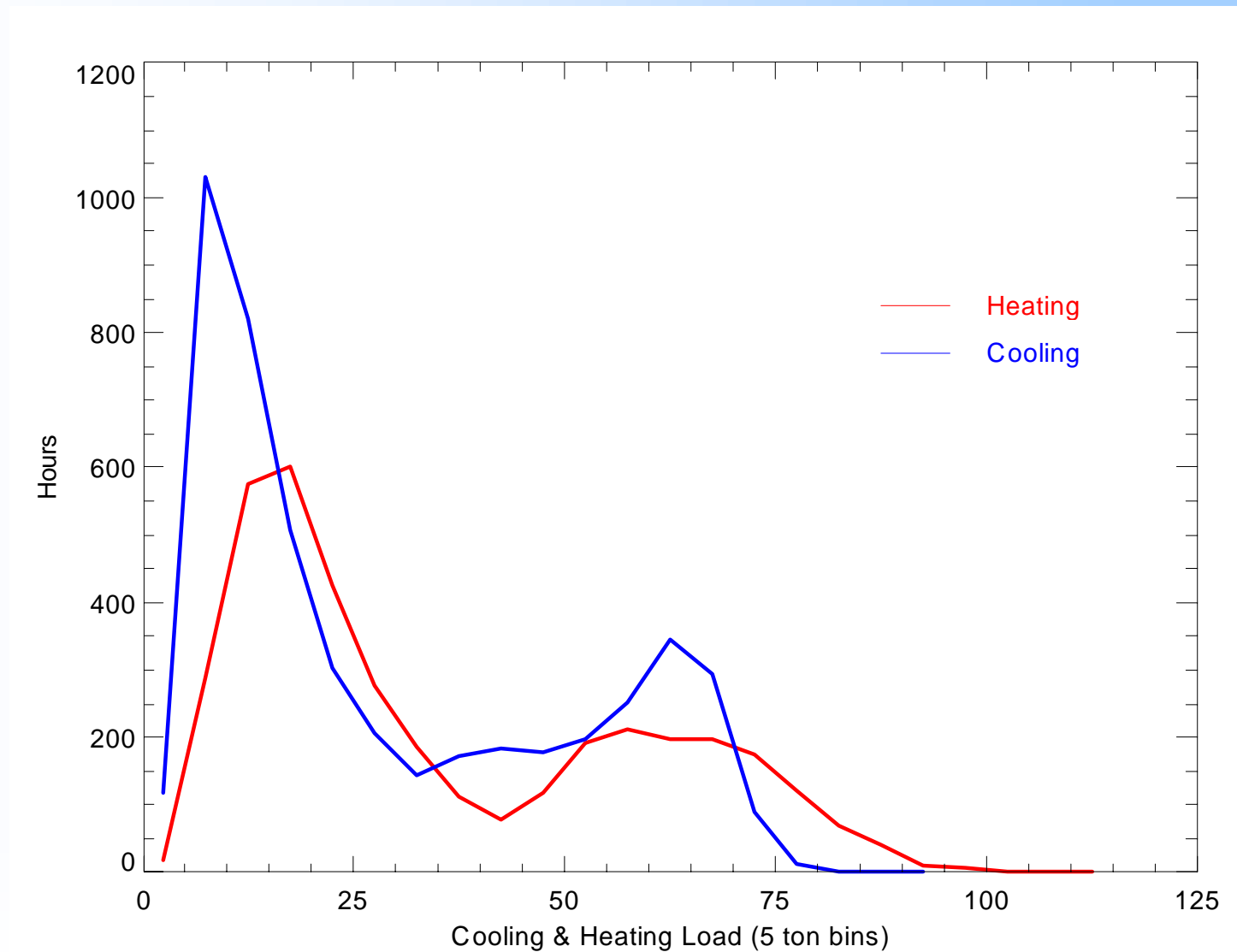


- Used heating/cooling status data with known HP sizes
- Adjusted HP capacity data based on loop temperatures i.e., $CAP(T)$
- Also calculated (and measured) loop loading

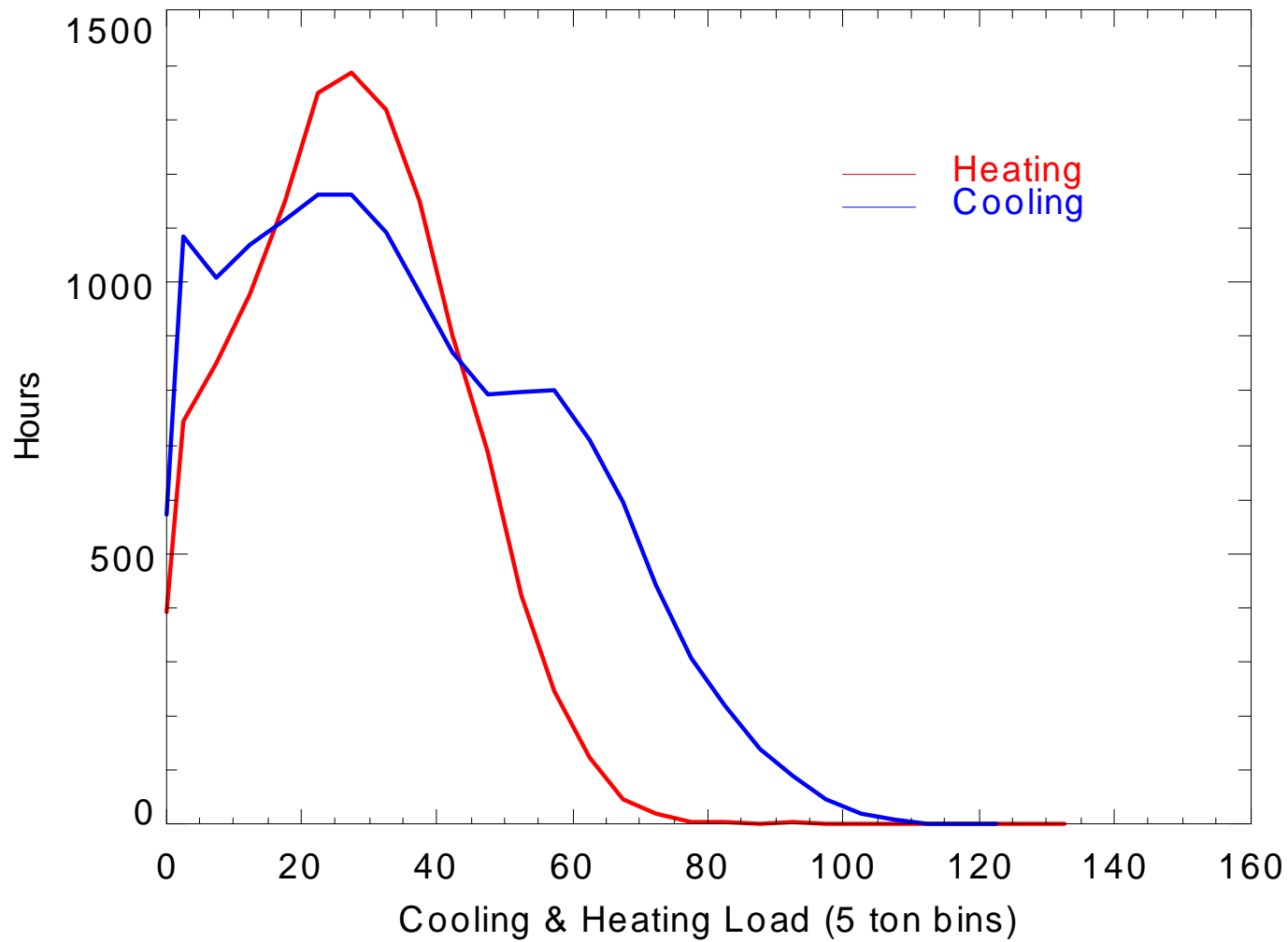
Sun Prairie Office (69 tons)



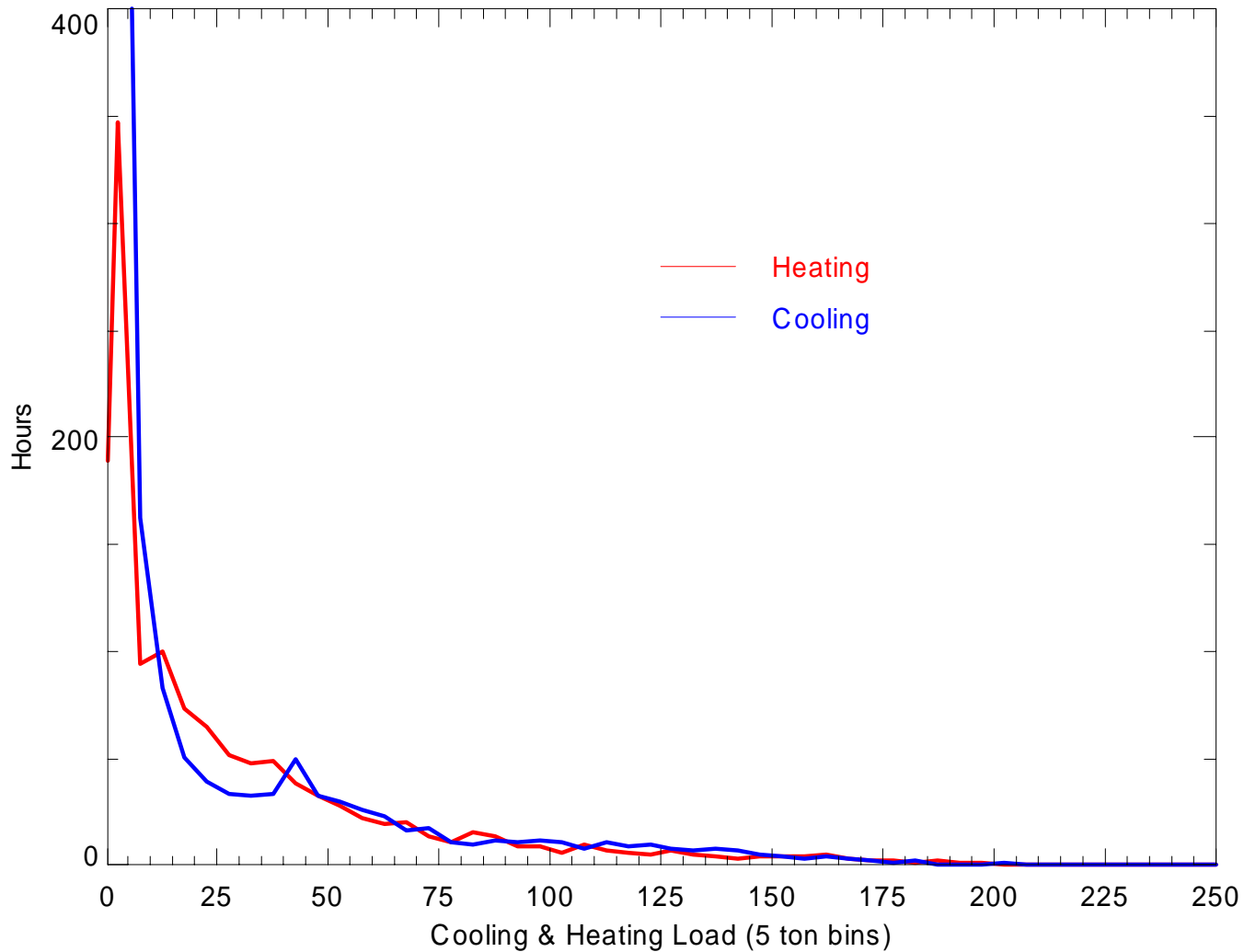
Middleton Office (146 tons)



Geneva Hotel (284 tons)



Johnson City School (400 tons)



Cooling Load Diversity

Hours at or Above Each Loading Level - Cooling

| Percent of Installed COOLING Capacity | Sun Prairie Office | Middleton Office | Geneva Hotel | High School |
|---|-----------------------|---------------------|--------------|-------------|
| 0% | 4,635 | 4,857 | 4,840 | 6,566 |
| 5% | 4,137 | 4,348 | 3,841 | 2,007 |
| 10% | 2,595 | 2,943 | 2,767 | 1,446 |
| 15% | 1,768 | 2,230 | 1,795 | 894 |
| 20% | 1,201 | 1,899 | 1,032 | 619 |
| 25% | 781 | 1,674 | 393 | 441 |
| 30% | 462 | 1,413 | 101 | 285 |
| 35% | 215 | 1,147 | 12 | 152 |
| 40% | 79 | 833 | - | 74 |
| 45% | 25 | 350 | - | 28 |
| 50% | 2 | 30 | - | 17 |
| 55% | - | 1 | - | 4 |
| 60% | - | - | - | 1 |

Heating Load Diversity

Hours at or Above Each Loading Level - Heating

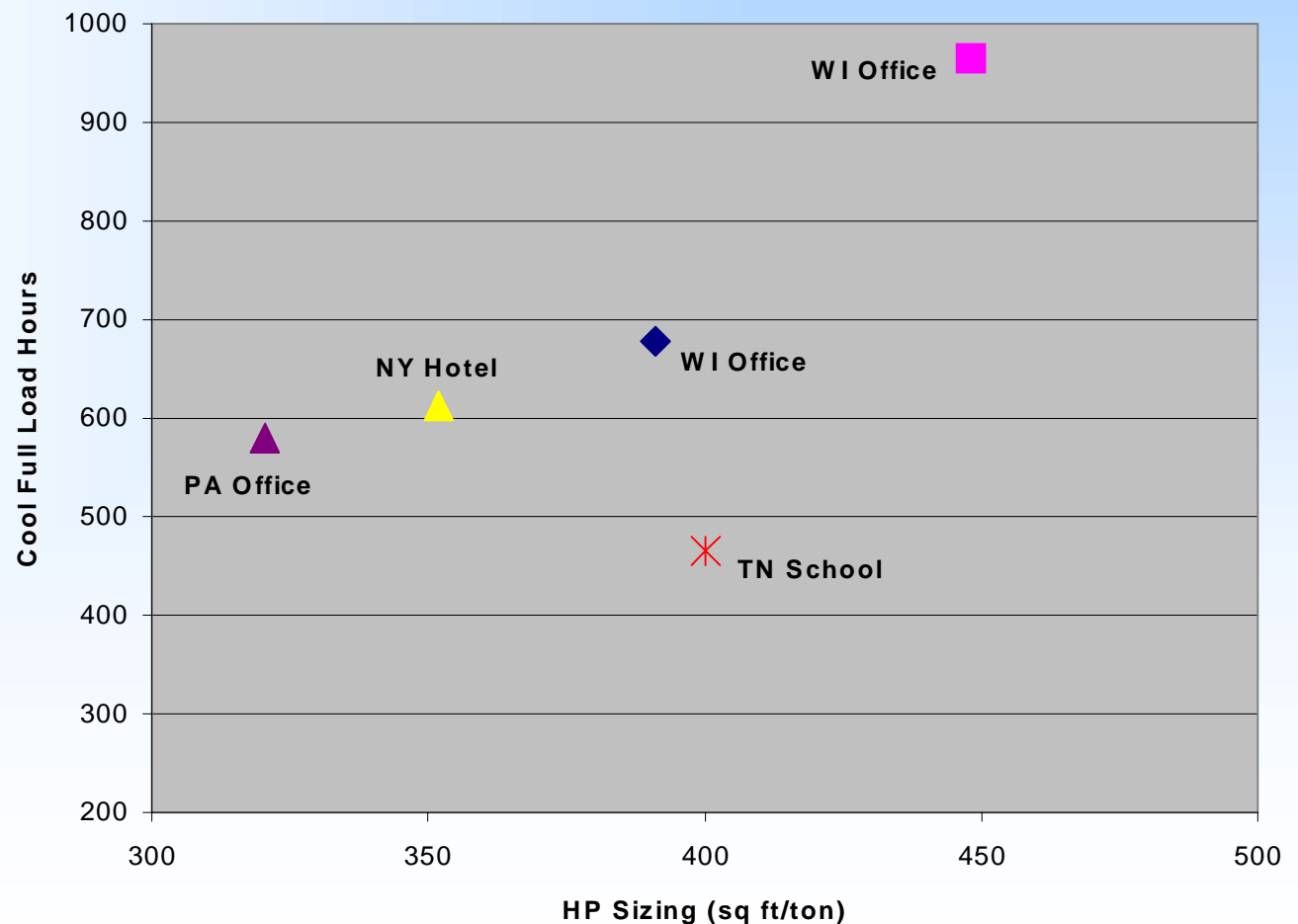
| Percent of Installed HEATING Capacity | Sun Prairie Office | Middleton Office | Geneva Hotel | High School |
|--|-------------------------------|-----------------------------|---------------------|--------------------|
| 0% | 3,957 | 3,903 | 3,804 | 4,596 |
| 5% | 3,779 | 3,751 | 3,001 | 2,384 |
| 10% | 2,418 | 2,906 | 1,799 | 1,599 |
| 15% | 1,106 | 2,093 | 664 | 1,054 |
| 20% | 489 | 1,649 | 119 | 745 |
| 25% | 240 | 1,432 | 14 | 545 |
| 30% | 114 | 1,291 | 5 | 388 |
| 35% | 50 | 1,014 | 2 | 288 |
| 40% | 12 | 689 | - | 208 |
| 45% | 2 | 382 | - | 148 |
| 50% | - | 150 | - | 92 |
| 55% | - | 39 | - | 51 |
| 60% | - | 9 | - | 28 |
| 65% | - | 1 | - | - |

Heating/Cooling Load Summary

| | Sun Prairie Office | Middleton Office | Geneva Hotel | Johnson City High School |
|--------------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
| Peak Hourly / 4-hr Cooling Loads: | 34 / 32 tons | 82 / 74 tons | 106 / 101 tons | 234 / 219 tons |
| % of Installed Cooling Capacity | 49% / 47% | 57% / 50% | 37% / 35% | 58% / 55% |
| Equivalent Full Load Hours – Cooling | 679 hours | 965 hours | 613 hours | 466 hours |
| Equivalent Full Load Hours – Heating | 504 hours | 869 hours | 372 hours | 318 hours |
| Normalized Cooling Loads | 1.7 ton-h/ft ² -yr | 2.2 ton-h/ft ² -yr | 1.7 ton-h/ft ² -yr | 1.2 ton-h/ft ² -yr |

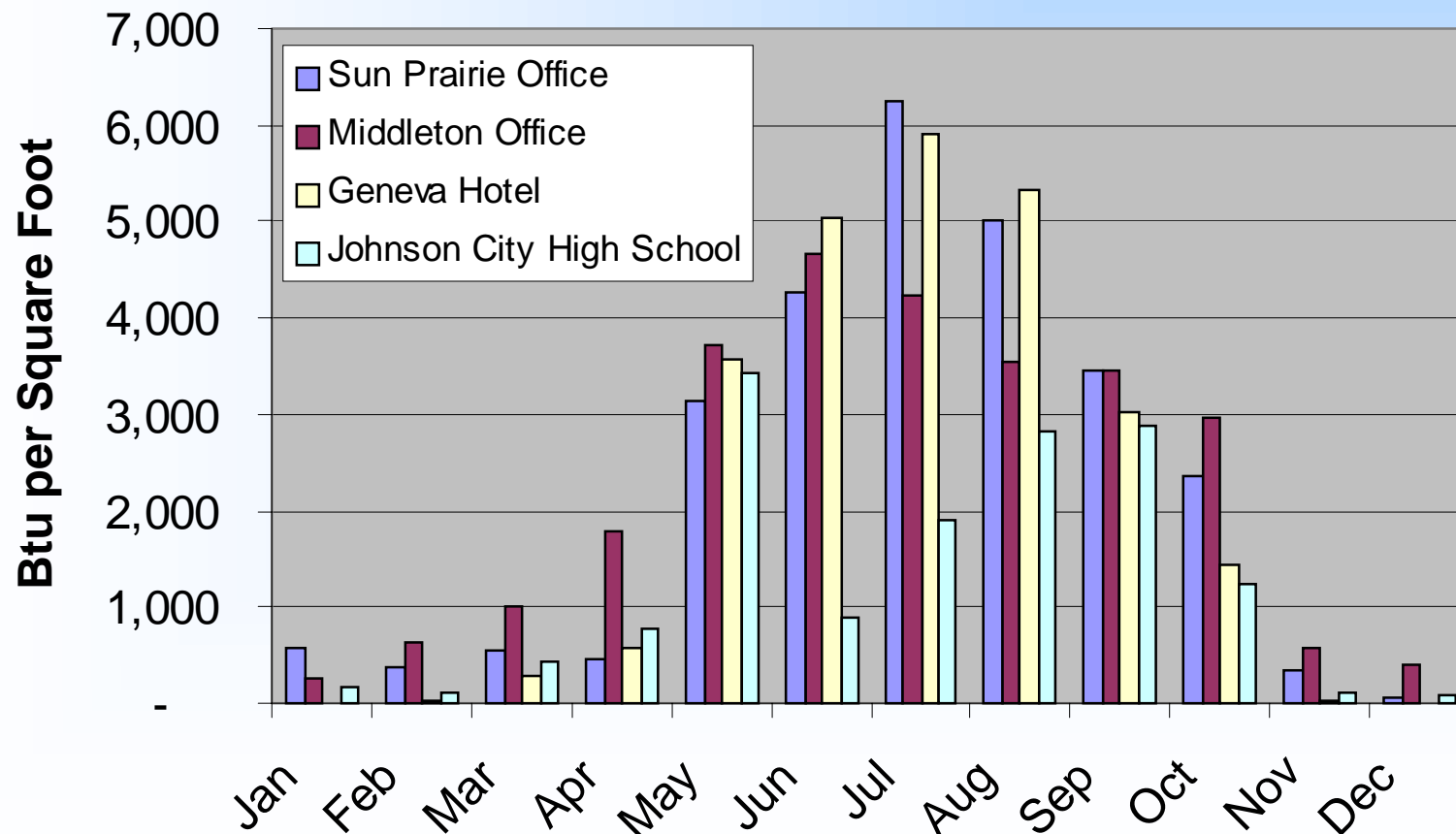
Are Full Load Hours the Right “Rule of Thumb” ?

- Full load hours (FLH) depend on sizing
- Norm. cooling loads are more consistent



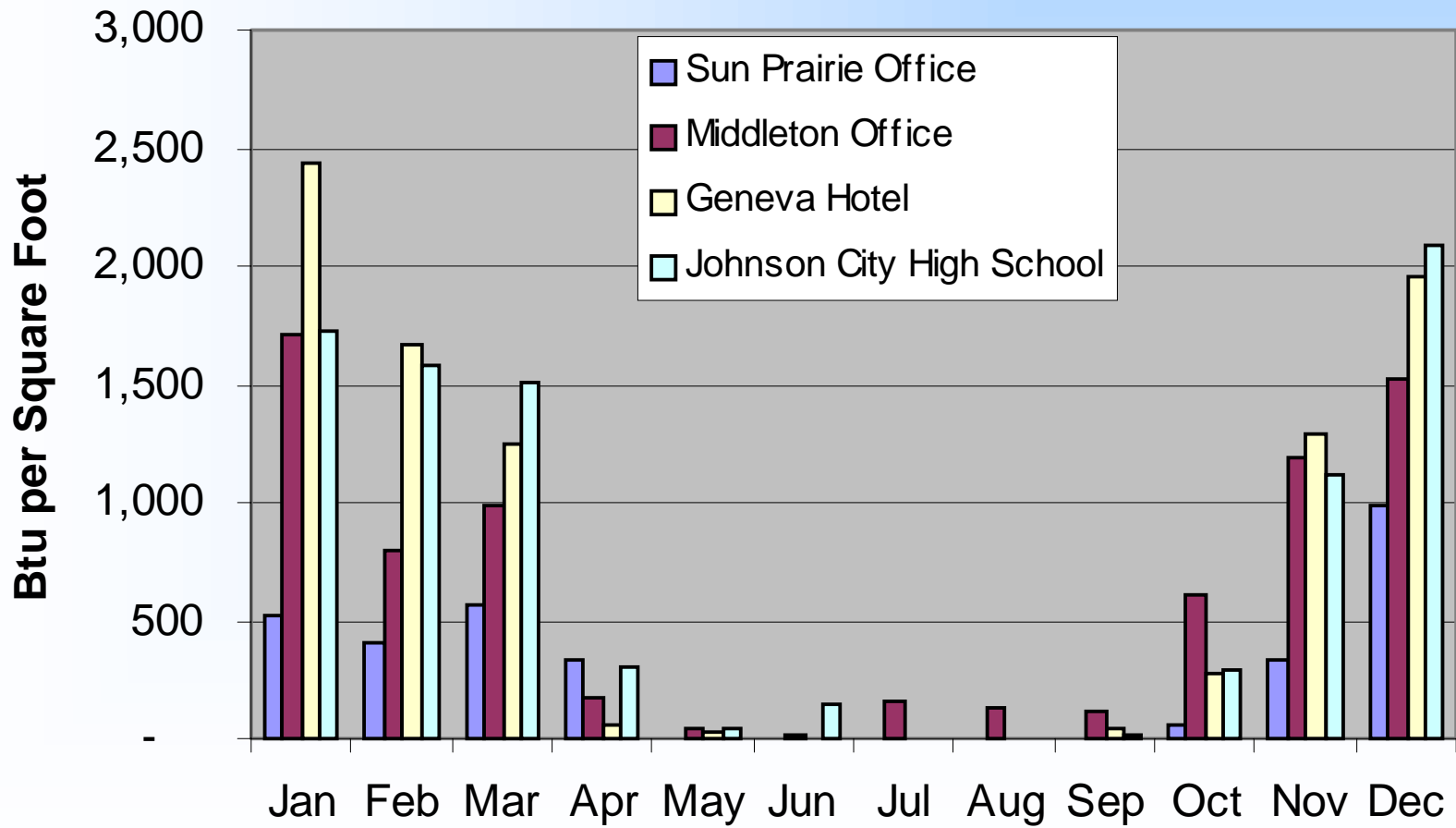
Heat Rejection - All Sites

Monthly Heat Rejection



Heat Extraction - All Sites

Monthly Heat Extraction

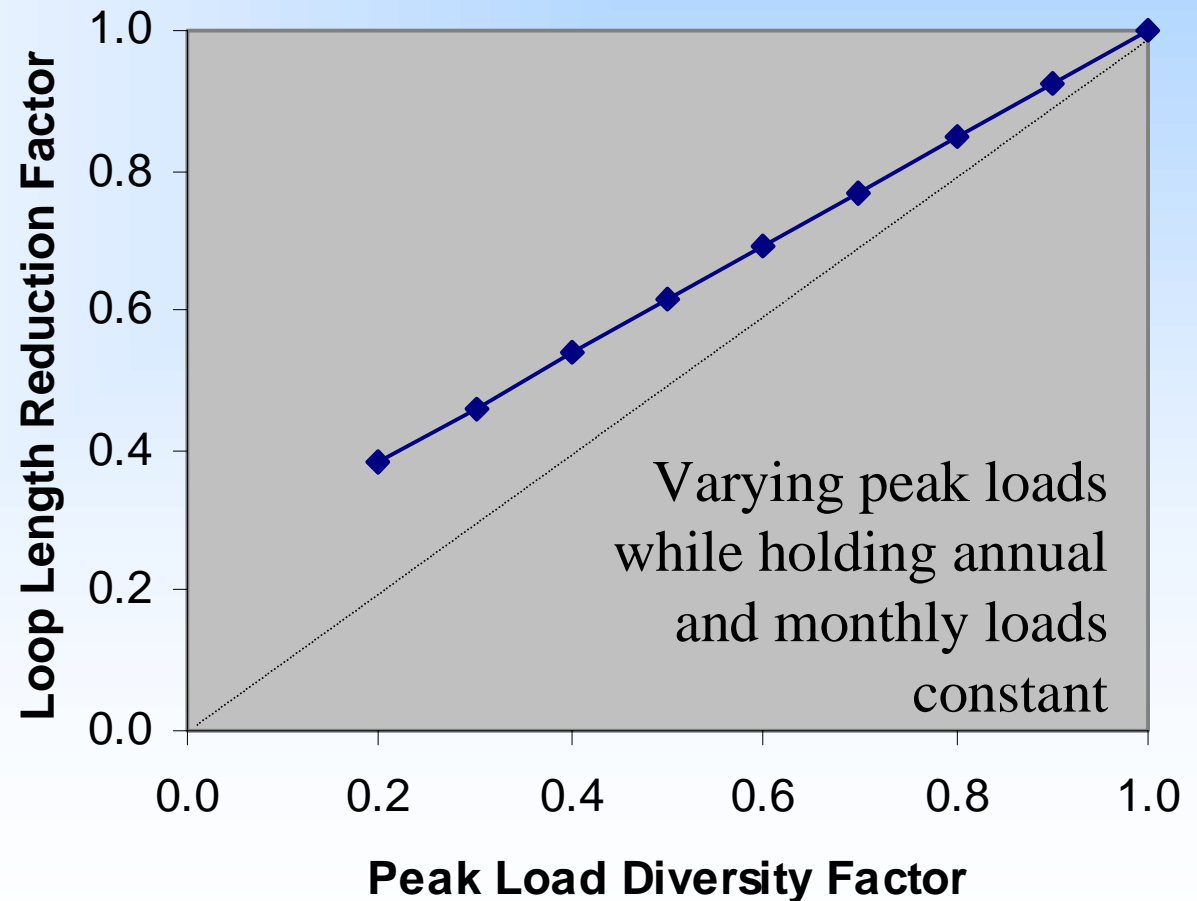


Loop Load Summary

| | Sun Prairie Office | Middleton Office | Geneva Hotel | Johnson City High School |
|--|---------------------------|-------------------------|---------------------|---------------------------------|
| Peak Hourly / 4-hr Heat Rejection (Btu/h-ft ²) | 22.2 / 20.5 | 42.5 / 29.9 | 15.6 / 14.8 | 22.5 / 20.6 |
| Peak Hourly / 4-hr Heat Extraction (Btu/h-ft ²) | 6.2 / 4.7 | 23.4 / 12.2 | 8.7 / 7.1 | 13.3 / 11.1 |
| Normalized Annual Heat Rejection (MBtu/yr-ft ²) | 26.8 | 27.3 | 25.2 | 14.8 |
| Normalized Annual Heat Extraction (MBtu/yr-ft ²) | 3.3 | 7.5 | 8.9 | 8.8 |

Implications of Load Diversity on Ground Loop Sizing

- ASHRAE loop sizing procedure shows loop length is mostly a function of peak loads



Summary of Findings

- Peak cooling loads were 40 to 60% of installed capacity...high diversity
- Loads found to be similar for diverse mix of buildings... schools being the exception
- Cooling full load hours (FLH) ranged from 466 to 965...though but may not be the best rule of thumb
- Load diversity has significant implications on loop sizing...using 50% diversity factor would allow 40% reduction in loop size